

A tool for distinguishing different neutrinoless double beta mechanisms

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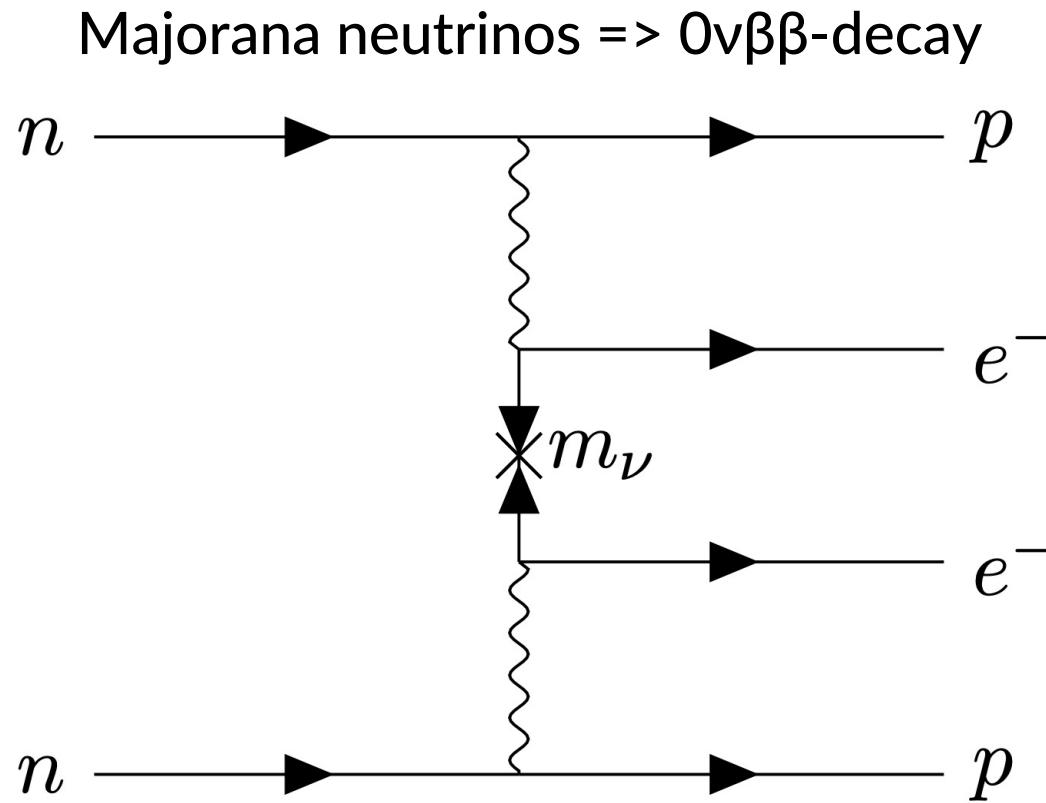
Max Planck Institute for Nuclear Physics, Heidelberg

Overview

What we will discuss:

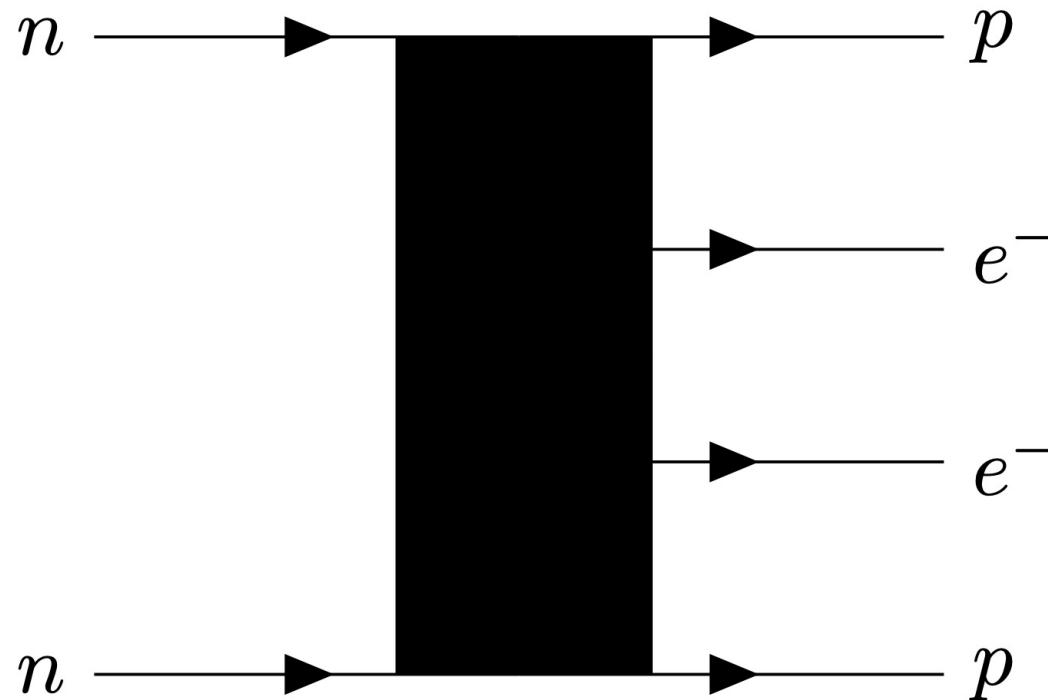
- Classification of $0\nu\beta\beta$ mechanisms (standard vs non-standard)
- Brief summary of EFT framework
- Ways to distinguish different mechanisms
- A generalized online tool

0νββ standard mechanism



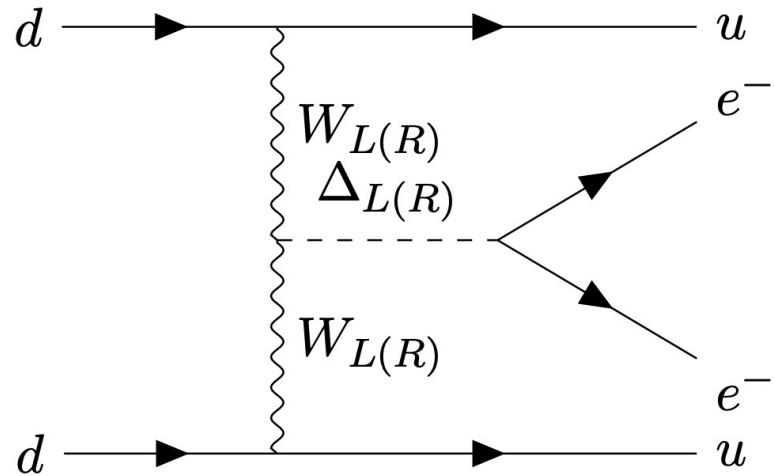
$0\nu\beta\beta$ standard mechanism?

Majorana neutrinos => $0\nu\beta\beta$ -decay

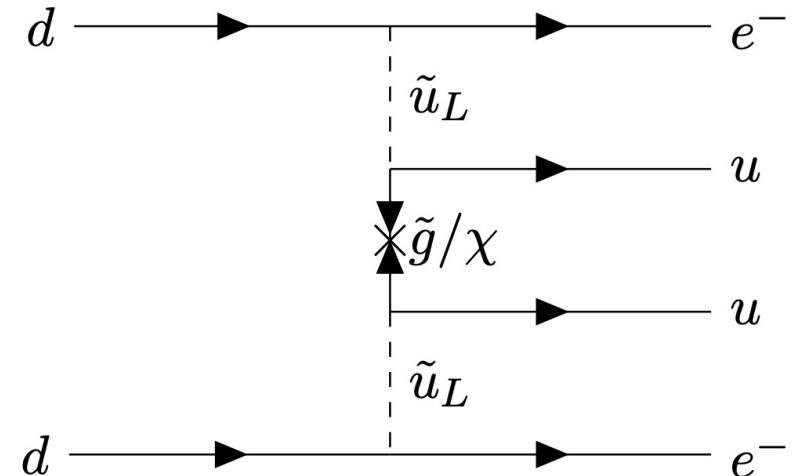


$0\nu\beta\beta$ non-standard mechanisms

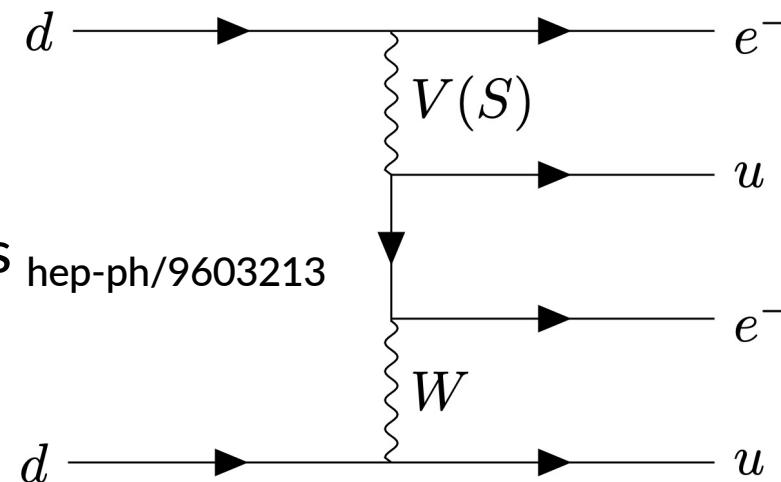
Scalars in minimal LR symmetry



R_P -violating SUSY Phys. Rev. Lett. 75, 17



Leptoquarks hep-ph/9603213



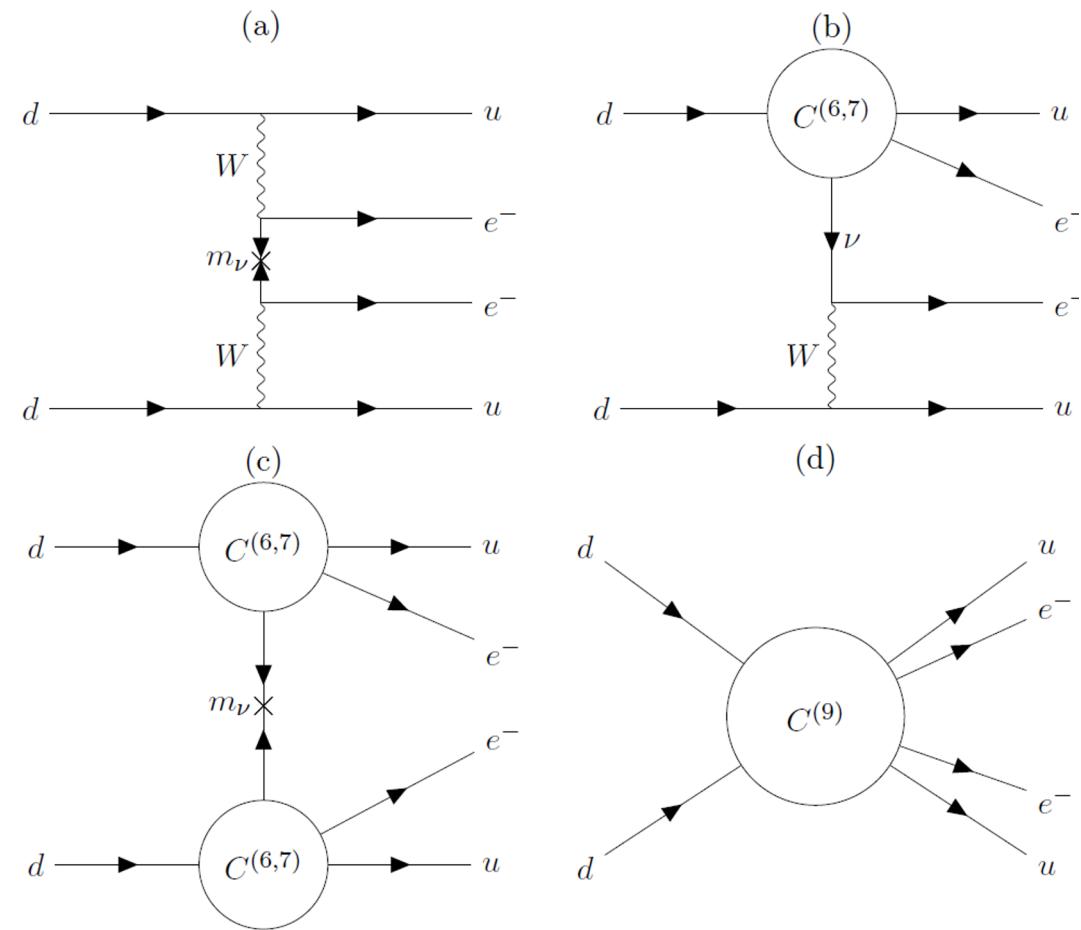
$0\nu\beta\beta$ mechanisms -Classification

a) mass mechanism

b) long-range

c) ignore_(suppressed)

d) short-range



EFT Approach [Cirigliano et al. ArXiv:1806.02780]

Low-Energy decay process

→ use LEFT (no light new physics!)

32 different operators

1 mass mechanism (dim 3)

7 long-range (dim 6,7)

24 short-range (dim 9)

Class	Op. Name	Op. Structure
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Dim 3		
Ψ^2	$\mathcal{O}_{m_{\beta\beta}}$	$-\frac{1}{2} m_{ee} \bar{\nu}_{L,e}^C \nu_{L,e}$

Dim 6		
Ψ^4	$\mathcal{O}_{SL}^{(6)}$ $\mathcal{O}_{SR}^{(6)}$ $\mathcal{O}_{VL}^{(6)}$ $\mathcal{O}_{VR}^{(6)}$ $\mathcal{O}_T^{(6)}$	$[\bar{u}_R d_L] [\bar{e}_L \nu_L^C]$ $[\bar{u}_L d_R] [\bar{e}_L \nu_L^C]$ $[\bar{u}_L \gamma^\mu d_L] [\bar{e}_R \gamma_\mu \nu_L^C]$ $[\bar{u}_R \gamma^\mu d_R] [\bar{e}_R \gamma_\mu \nu_L^C]$ $[\bar{u}_L \sigma^{\mu\nu} d_R] [\bar{e}_L \sigma_{\mu\nu} \nu_L^C]$

Dim 7		
$\Psi^4 \partial$	$\mathcal{O}_{VL}^{(7)}$ $\mathcal{O}_{VR}^{(7)}$	$[\bar{u}_L \gamma^\mu d_L] [\bar{e}_L \overset{\leftrightarrow}{\partial}_\mu \nu_L^C]$ $[\bar{u}_R \gamma^\mu d_R] [\bar{e}_L \partial_\mu \nu_L^C]$

Dim 9		
Ψ^6	$\mathcal{O}_{1L,R}^{(9)}, \mathcal{O}_{1L,R}'$ $\mathcal{O}_{2L,R}^{(9)}, \mathcal{O}_{2L,R}'$ $\mathcal{O}_{3L,R}^{(9)}, \mathcal{O}_{3L,R}'$ $\mathcal{O}_{4L,R}^{(9)}$ $\mathcal{O}_{5L,R}^{(9)}$ $\mathcal{O}_6^{(9)}$ $\mathcal{O}_7^{(9)'}$ $\mathcal{O}_8^{(9)'}$ $\mathcal{O}_9^{(9)'}$ $\mathcal{O}_9^{(9)''}$	$[\bar{u}_L \gamma_\mu d_L] [\bar{u}_L \gamma^\mu d_L] [\bar{e}_{L,R} e_{L,R}^C]$ $[\bar{u}_R \gamma_\mu d_R] [\bar{u}_R \gamma^\mu d_R] [\bar{e}_{L,R} e_{L,R}^C]$ $[\bar{u}_R d_L] [\bar{u}_R d_L] [\bar{e}_{L,R} e_{L,R}^C]$ $[\bar{u}_L d_R] [\bar{u}_L d_R] [\bar{e}_{L,R} e_{L,R}^C]$ $[\bar{u}_R^\alpha d_L^\beta] [\bar{u}_R^\beta d_L^\alpha] [\bar{e}_{L,R} e_{L,R}^C]$ $[\bar{u}_L^\alpha d_R^\beta] [\bar{u}_L^\beta d_R^\alpha] [\bar{e}_{L,R} e_{L,R}^C]$ $[\bar{u}_L \gamma^\mu d_L] [\bar{u}_R \gamma_\mu d_R] [\bar{e}_{L,R} e_{L,R}^C]$ $[\bar{u}_L^\alpha \gamma^\mu d_L^\beta] [\bar{u}_R^\beta \gamma_\mu d_R^\alpha] [\bar{e}_{L,R} e_{L,R}^C]$ $[\bar{u}_L \gamma_\mu d_L] [\bar{u}_L d_R] [\bar{e} \gamma^\mu \gamma_5 e^C]$ $[\bar{u}_R \gamma_\mu d_R] [\bar{u}_R d_L] [\bar{e} \gamma^\mu \gamma_5 e^C]$ $[\bar{u}_L t^A \gamma_\mu d_L] [\bar{u}_R t^A d_R] [\bar{e} \gamma^\mu \gamma_5 e^C]$ $[\bar{u}_R t^A \gamma_\mu d_R] [\bar{u}_R t^A d_L] [\bar{e} \gamma^\mu \gamma_5 e^C]$ $[\bar{u}_L \gamma_\mu d_L] [\bar{u}_R d_L] [\bar{e} \gamma^\mu \gamma_5 e^C]$ $[\bar{u}_R \gamma_\mu d_R] [\bar{u}_L d_R] [\bar{e} \gamma^\mu \gamma_5 e^C]$ $[\bar{u}_L t^A \gamma_\mu d_L] [\bar{u}_R t^A d_L] [\bar{e} \gamma^\mu \gamma_5 e^C]$ $[\bar{u}_R t^A \gamma_\mu d_R] [\bar{u}_L t^A d_R] [\bar{e} \gamma^\mu \gamma_5 e^C]$

EFT Approach [Cirigliano et al. ArXiv:1806.02780]

Standard Formula

$$\left(T_{1/2}^{0\nu}\right)^{-1} = |m_{\beta\beta}|^2 |\mathcal{M}^{0\nu}|^2 G^{0\nu}(Q, Z)$$



0νββ “Master-Formula”

$$\begin{aligned} \left(T_{1/2}^{0\nu}\right)^{-1} = & g_A^4 \left[G_{01} \left(|\mathcal{A}_\nu|^2 + |\mathcal{A}_R|^2 \right) - 2(G_{01} - G_{04}) \operatorname{Re} [\mathcal{A}_\nu^* \mathcal{A}_R] \right. \\ & + 4G_{02} |\mathcal{A}_E|^2 + 2G_{04} \left(|\mathcal{A}_{m_e}|^2 + \operatorname{Re} [\mathcal{A}_{m_e}^* (\mathcal{A}_\nu + \mathcal{A}_R)] \right) \\ & - 2G_{03} \operatorname{Re} [(\mathcal{A}_\nu + \mathcal{A}_R) \mathcal{A}_E^* + 2\mathcal{A}_{m_e} \mathcal{A}_E^*] \\ & \left. + G_{09} |\mathcal{A}_M|^2 + G_{06} \operatorname{Re} [(\mathcal{A}_\nu - \mathcal{A}_R) \mathcal{A}_M^*] \right] \end{aligned}$$

Input: Wilson Coefficients + 3 numerical inputs (NMEs, PSFs, LECs)

EFT Approach [Cirigliano et al. ArXiv:1806.02780]

Standard Formula

$$\left(T_{1/2}^{0\nu}\right)^{-1} = |m_{\beta\beta}|^2 |\mathcal{M}^{0\nu}|^2 G^{0\nu}(Q, Z)$$



0νββ “N_A_ν = $\frac{m_{\beta\beta}}{m_e} \mathcal{M}_\nu^{(3)}$ Formula”

$$\begin{aligned}
 \left(T_{1/2}^{0\nu}\right)^{-1} = & \frac{m_{\beta\beta}}{m_e} \mathcal{M}_\nu^{(3)} + \frac{m_N}{m_e} \mathcal{M}_\nu^{(2)} - 2(G_{01} - G_{04}) \operatorname{Re} [\mathcal{A}_\nu^* \mathcal{A}_R] \\
 & + \frac{m_N^2}{m_e v} \mathcal{M}_\nu^{(6)} \left(C_{SL}^{(6)}, C_{SR}^{(6)}, C_T^{(6)}, C_{VL}^{(7)}, C_{VR}^{(7)} \right) \operatorname{Re} [\mathcal{A}_\nu^* (\mathcal{A}_\nu + \mathcal{A}_R)] \\
 & - 2G_{03} \operatorname{Re} [\mathcal{A}_\nu^* \mathcal{A}_L] \left(C_{1L}^{(9)}, C_{1L}'^{(9)}, C_{2L}^{(9)}, C_{2L}'^{(9)}, C_{3L}^{(9)}, C_{3L}'^{(9)}, C_{4L}^{(9)}, C_{5L}^{(9)} \right) \\
 & + G_{09} |\mathcal{A}_M|^2 + G_{06} \operatorname{Re} [(\mathcal{A}_\nu^* \mathcal{A}_R) \left(C_{1L}^{(9)}, C_{1L}'^{(9)}, C_{2L}^{(9)}, C_{2L}'^{(9)}, C_{3L}^{(9)}, C_{3L}'^{(9)}, C_{4L}^{(9)}, C_{5L}^{(9)} \right)]
 \end{aligned}$$

Input: Wilson Coefficients + 3 numerical inputs (NM_L, LECs)

EFT Approach [Cirigliano et al. ArXiv:1806.02780]

Standard Formula

$$\left(T_{1/2}^{0\nu}\right)^{-1} = |m_{\beta\beta}|^2 |\mathcal{M}^{0\nu}|^2 G^{0\nu}(Q, Z)$$



0νββ “ $\mathcal{A}_\nu = \frac{m_{\beta\beta}}{m_e} \mathcal{M}_\nu^{(3)}$ ”

$$\left(T_{1/2}^{0\nu}\right)^{-1} = \frac{m_N^2}{m_e v} \mathcal{M}_R^{(9)} \left(C_{1R}^{(9)}, C_{1R}^{(9)\prime}, C_{2R}^{(9)}, C_{2R}^{(9)\prime}, C_{3R}^{(9)}, C_{3R}^{(9)\prime}, C_{4R}^{(9)}, C_{5R}^{(9)} \right),$$

$$\mathcal{A}_R = \frac{m_N^2}{m_e v} \mathcal{M}_R^{(9)} \left(C_{1R}^{(9)}, C_{1R}^{(9)\prime}, C_{2R}^{(9)}, C_{2R}^{(9)\prime}, C_{3R}^{(9)}, C_{3R}^{(9)\prime}, C_{4R}^{(9)}, C_{5R}^{(9)} \right),$$

$$\mathcal{A}_E = \mathcal{M}_{E,L}^{(6)} \left(C_{VL}^{(6)} \right) + \mathcal{M}_{E,R}^{(6)} \left(C_{VR}^{(6)} \right),$$

$$\mathcal{A}_{me} = \mathcal{M}_{me,L}^{(6)} \left(C_{VL}^{(6)} \right) + \mathcal{M}_{me,R}^{(6)} \left(C_{VR}^{(6)} \right),$$

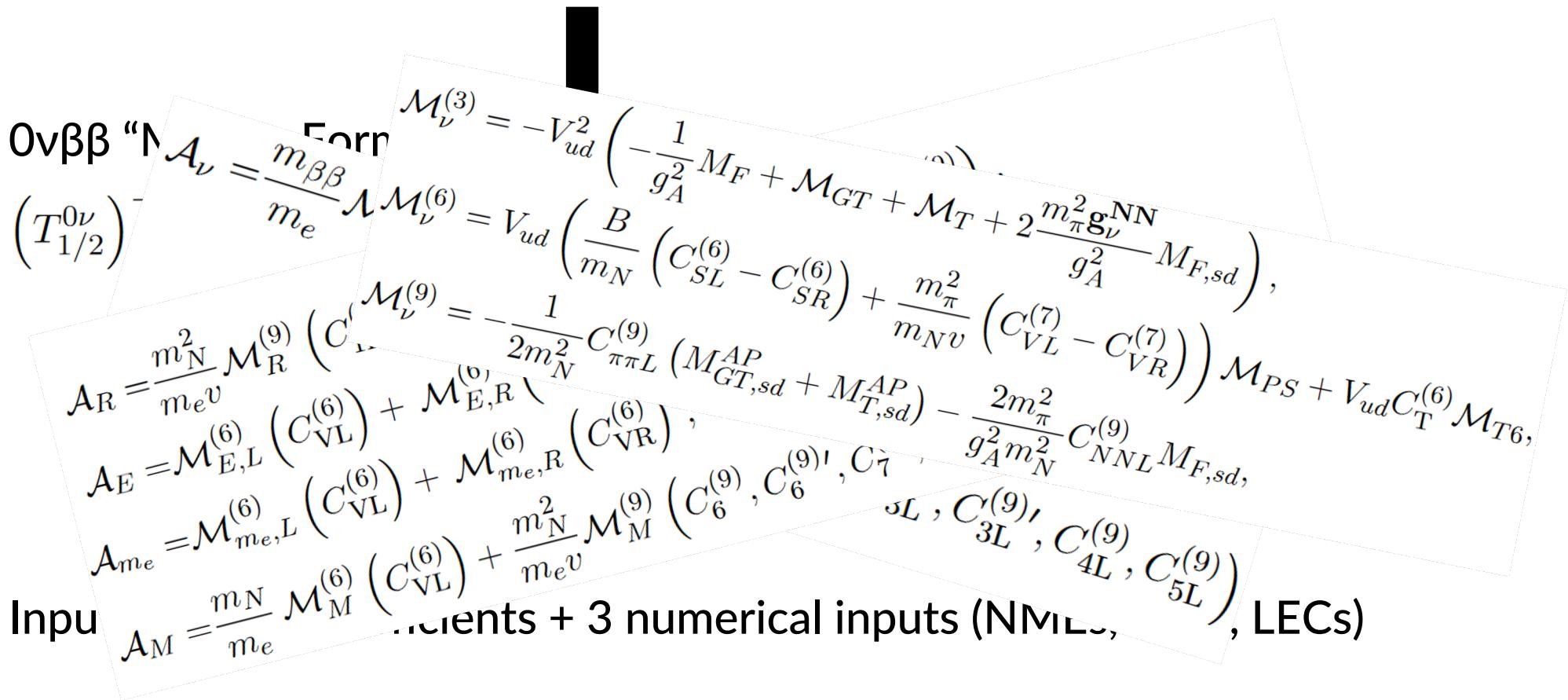
$$\mathcal{A}_M = \frac{m_N}{m_e} \mathcal{M}_M^{(6)} \left(C_{VL}^{(6)} \right) + \frac{m_N^2}{m_e v} \mathcal{M}_M^{(9)} \left(C_6^{(9)}, C_6^{(9)\prime}, C_7^{(9)}, C_7^{(9)\prime}, C_8^{(9)}, C_8^{(9)\prime}, C_9^{(9)}, C_9^{(9)\prime} \right),$$

Input parameters + 3 numerical inputs (N_{MLJ} , LECs)

EFT Approach [Cirigliano et al. ArXiv:1806.02780]

Standard Formula

$$\left(T_{1/2}^{0\nu}\right)^{-1} = |m_{\beta\beta}|^2 |\mathcal{M}^{0\nu}|^2 G^{0\nu}(Q, Z)$$



EFT Approach [Cirigliano et al. ArXiv:1806.02780]

Standard Formula

$$\left(T_{1/2}^{0\nu}\right)^{-1} = |m_{\beta\beta}|^2 |\mathcal{M}^{0\nu}|^2 G^{0\nu}(Q, Z)$$

0νββ “N”

$$\mathcal{A}_\nu = \frac{m_{\beta\beta}}{m_e} \mathcal{M}^{(6)} \quad \mathcal{M}_\nu^{(3)} = -V_{ud}^2 \left(-\frac{1}{g_A^2} M_F + \mathcal{M}_{E,L}^{(3)} \right) \quad \mathcal{M}_\nu^{(6)} = V_{ud} \left(\frac{B}{m_N} \left(\mathcal{M}_{E,L}^{(6)} = -\frac{V_{ud} C_{VL}^{(6)}}{3} \left(\frac{g_V^2}{g_A^2} M_F + \frac{1}{3} (2M_{GT}^{AA} + M_T^{AA}) + \frac{6g_{VL}^E}{g_A^2} M_{F,sd} \right), \right. \right.$$

$$\left. \left. \mathcal{M}_{E,R}^{(6)} = -\frac{V_{ud} C_{VR}^{(6)}}{3} \left(\frac{g_V^2}{g_A^2} M_F - \frac{1}{3} (2M_{GT}^{AA} + M_T^{AA}) + \frac{6g_{VR}^E}{g_A^2} M_{F,sd} \right), \right. \right. \\ \mathcal{M}_\nu^{(9)} = -\frac{1}{2m_N^2} C_{\pi\pi L}^{(9)} \quad \mathcal{M}_{E,R}^{(6)} = -\frac{V_{ud} C_{VR}^{(6)}}{3} \left(\frac{g_V^2}{g_A^2} M_F - \frac{1}{3} (2M_{GT}^{AA} + M_T^{AA}) + \frac{6g_{VR}^E}{g_A^2} M_{F,sd} \right) \left(\mathcal{M}_{PS} + V_{ud} C_T^{(6)} \mathcal{M}_{T6} \right), \\ \mathcal{A}_R = \frac{m_N^2}{m_e v} \mathcal{M}_R^{(9)} \quad \mathcal{A}_L = \frac{m_N^2}{m_e v} \mathcal{M}_L^{(9)} \quad \mathcal{A}_{AP} = M_{T,sd}^{AP} - \frac{2m_\pi^2}{g_A^2 m_N^2} C_{NNL}^{(9)} M_{F,sd}, \\ \mathcal{A}_E = \mathcal{M}_{E,L}^{(6)} \left(C_{VL}^{(6)} \right) + \mathcal{M}_{E,R}^{(6)} \left(C_{VR}^{(6)} \right), \quad \mathcal{A}_{me} = \mathcal{M}_{me,L}^{(6)} \left(C_{VL}^{(6)} \right) + \mathcal{M}_{me,R}^{(6)} \left(C_{VR}^{(6)} \right), \quad \mathcal{A}_M = \frac{m_N}{m_e} \mathcal{M}_M^{(6)} \left(C_{VL}^{(6)} \right) + \frac{m_N^2}{m_e v} \mathcal{M}_M^{(9)} \left(C_6^{(9)}, C_6^{(9)\prime}, C_7^{(9)}, C_{2L}^{(9)}, C_{3L}^{(9)}, C_{4L}^{(9)}, C_{5L}^{(9)} \right), \\ \text{Input parameters + 3 numerical inputs (NMLECs, LECs)}$$

EFT Approach [Cirigliano et al. ArXiv:1806.02780]

Standard Formula

$$\left(T_{1/2}^{0\nu}\right)^{-1} = |m_{\beta\beta}|^2 |\mathcal{M}^{0\nu}|^2 G^{0\nu}(Q, Z)$$

0νββ “N”

$$\mathcal{A}_\nu = \frac{m_{\beta\beta}}{m_e} \mathcal{M}^{(6)} \quad \mathcal{M}_\nu^{(3)} = -V_{ud}^2 \left(-\frac{1}{g_A^2} M_F + \mathcal{M}_{\text{corr}}^{(3)} \right),$$

$$\left(T_{1/2}^{0\nu}\right)^{-1} = \frac{B}{m_N} \left(\mathcal{M}_{E,L}^{(6)} - \frac{V_{ud} C_{VL}^{(6)}}{3} \left(\frac{g_V^2}{g_A^2} M_F + \frac{1}{3} (2M_{GT}^{AA} + M_T^{AA}) + \frac{6g_{VL}^E}{g_A^2} M_{F,sd} \right) \right),$$

$$\mathcal{A}_R = \frac{m_N^2}{m_e v} \mathcal{M}_R^{(9)} \left(C_R^{(9)} \right),$$

$$\mathcal{A}_L = \frac{m_N^2}{m_e v} \mathcal{M}_L^{(9)} \left(C_L^{(9)} \right),$$

$$\mathcal{A}_E = \mathcal{M}_{E,L}^{(6)} \left(C_{VL}^{(6)} \right) + \mathcal{M}_{m_e,L}^{(6)} \left(C_{VR}^{(6)} \right),$$

$$\mathcal{A}_{m_e} = \mathcal{M}_{m_e,L}^{(6)} \left(C_{VL}^{(6)} \right) + \mathcal{M}_{m_e,R}^{(6)} \left(C_{VR}^{(6)} \right),$$

Input

$$\mathcal{A}_M = \frac{m_N}{m_e} \mathcal{M}_M^{(6)} \left(C_M^{(6)} \right),$$

$$\mathcal{M}_{E,L}^{(6)} = V_{ud} C_{VL}^{(6)} \left(\frac{g_V^2}{g_A^2} M_F - \frac{1}{3} (M_{GT}^{AA} - 4M_T^{AA}) - 3(M_{GT}^{AP} + M_{GT}^{PP} + M_T^{AP} + M_T^{PP}) \right) \mathcal{M}_{T6},$$

$$-\frac{12g_{VL}^m}{g_A^2} M_{F,sd} \right),$$

$$\mathcal{M}_{m_e,R}^{(6)} = V_{ud} C_{VR}^{(6)} \left(\frac{g_V^2}{g_A^2} M_F + \frac{1}{3} (M_{GT}^{AA} - 4M_T^{AA}) + 3(M_{GT}^{AP} + M_{GT}^{PP} + M_T^{AP} + M_T^{PP}) \right) \mathcal{M}_{T6},$$

$$-\frac{12g_{VR}^m}{g_A^2} M_{F,sd} \right),$$

EFT Approach [Cirigliano et al. ArXiv:1806.02780]

Standard Formula

$$\left(T_{1/2}^{0\nu}\right)^{-1} = |m_{\beta\beta}|^2 |\mathbf{M}^{0\nu}|^2 G^{0\nu}(Q, Z)$$

0νββ “N”

$$\mathcal{A}_\nu = \frac{m_e}{m_e}$$

$$\left(T_{1/2}^{0\nu}\right)^{-1} = \frac{m_\pi^2}{m_N^2} \left[-\frac{2}{g_A^2} (g_6^{NN} C_V^{(9)} + g_7^{NN} \tilde{C}_V^{(9)}) M_{F,sd} + \frac{1}{2} (g_V^{\pi N} C_V^{(9)} + \tilde{g}_V^{\pi N} \tilde{C}_V^{(9)}) (M_{GT,sd}^{AP} + M_{T,sd}^{AP}) \right],$$

$$\mathcal{M}_M^{(6)} = V_{ud} C_{VL}^{(6)} \left[2 \frac{g_A}{g_M} (M_{GT}^{MM} + M_T^{MM}) + \frac{m_\pi^2}{m_N^2} \left(-\frac{2}{g_A^2} g_{VL}^{NN} M_{F,sd} + \frac{1}{2} g_{VL}^{\pi N} (M_{GT,sd}^{AP} + M_{T,sd}^{AP}) \right) \right],$$

$$\mathcal{M}_M^{(9)} = \frac{m_\pi^2}{m_N^2} \left[-\frac{2}{g_A^2} (g_6^{NN} C_V^{(9)} + g_7^{NN} \tilde{C}_V^{(9)}) (M_{GT,sd}^{AP} + M_{T,sd}^{AP}) + \frac{1}{2} (g_V^{\pi N} C_V^{(9)} + \tilde{g}_V^{\pi N} \tilde{C}_V^{(9)}) (M_{GT,sd}^{AP} + M_{T,sd}^{AP}) \right],$$

$$\mathcal{M}_{T6}^{(6)} = -\frac{V_{ud} C_{VR}^{(6)}}{3} \left(\frac{g_V^2}{g_A^2} M_F - \frac{1}{3} (2 M_{GT}^{AA} + M_T^{AA}) + \frac{6 g_{VL}^E}{g_A^2} M_{F,sd} \right),$$

$$\mathcal{M}_{T6}^{(9)} = \frac{g_V^2}{g_A^2} M_F - \frac{1}{3} (M_{GT}^{AA} - 4 M_T^{AA}) - 3 (M_{GT}^{AP} + M_{GT}^{PP} + M_T^{AP} + M_T^{PP}) \mathcal{M}_{T6},$$

Input

$$\mathcal{A}_M = \frac{m_N}{m_e} \mathcal{M}_M^{(6)} \left(C_R \right)$$

$$\mathcal{A}_R = \frac{m_N^2}{m_e v} \mathcal{M}_R^{(9)} \left(C_R \right)$$

$$\mathcal{A}_E = \mathcal{M}_{E,L}^{(6)} \left(C_{VL}^{(6)} \right)$$

$$\mathcal{A}_{me} = \mathcal{M}_{me,L}^{(6)} \left(C_{VL}^{(6)} \right)$$

$$\mathcal{M}_{me,R}^{(6)} = \frac{V_{ud} C_{VR}^{(6)}}{6} \left(\frac{g_V^2}{g_A^2} M_F + \frac{1}{3} (M_{GT}^{AA} - 4 M_T^{AA}) + 3 (M_{GT}^{AP} + M_{GT}^{PP} + M_T^{AP} + M_T^{PP}) - \frac{12 g_{VL}^{me}}{g_A^2} M_{F,sd} \right),$$

$$\mathcal{M}_{me,R}^{(9)} = \frac{g_V^2}{g_A^2} M_F - \frac{1}{3} (M_{GT}^{AA} - 4 M_T^{AA}) - 3 (M_{GT}^{AP} + M_{GT}^{PP} + M_T^{AP} + M_T^{PP}) - \frac{12 g_{VL}^{me}}{g_A^2} M_{F,sd},$$

EFT Approach [Cirigliano et al. ArXiv:1806.02780]

Simula

$$\mathcal{M}_{GT} = M_{GT}^{AA} + M_{GT}^{AP} + M_{GT}^{PP} + M_{GT}^{MM},$$

$$\mathcal{M}_T = M_T^{AP} + M_T^{PP} + M_T^{MM},$$

$$\mathcal{M}_{PS} = \frac{1}{2} M_{GT}^{AP} + M_{GT}^{PP} + \frac{1}{2} M_T^{AP} + M_T^{PP},$$

$$\mathcal{M}_{T6} = 2 \frac{\mathbf{g}'_T - \mathbf{g}_T^N}{g_A^2} \frac{m_\pi^2}{m_N^2} M_{F, sd} - \frac{8g_T}{g_M} (M_{GT}^{MM} + M_T^{MM})$$

$$+ \mathbf{g}_T^{\pi N} \frac{m_\pi^2}{4m_N^2} (M_{GT, sd}^{AP} + M_{T, sd}^{AP}) + \mathbf{g}_T^{\pi\pi} \frac{m_\pi^2}{4m_N^2} (M_{GT, sd}^{PP} + M_{T, sd}^{PP}).$$

($\pm 1/\omega$)

$$\mathcal{A}_R = \frac{m_N^2}{m_e v} \mathcal{M}_R^{(9)} (C_R)$$

$$\mathcal{A}_L = \mathcal{M}_{E,L}^{(6)} (C_{VL}^{(6)})$$

$$\mathcal{A}_E = \mathcal{M}_{E,L}^{(6)} (C_{VL}^{(6)})$$

$$\mathcal{A}_{me} = \mathcal{M}_{me,L}^{(6)} (C_{VL}^{(6)})$$

$$\mathcal{A}_M = \frac{m_N}{m_e} \mathcal{M}_M^{(6)} (C_M)$$

Inpu

$$\mathcal{M}_{me,R}^{(6)} = \frac{V_{ud} C_{VR}^{(6)}}{6} \left(\frac{g_V^2}{g_A^2} M_F + \frac{1}{3} (M_{GT}^{AA} - 4M_T^{AA}) + 3 (M_{GT}^{AP} + M_{GT}^{PP} + M_T^{AP} + M_T^{PP}) - \frac{12\mathbf{g}_{VL}^{me}}{g_A^2} M_{F, sd} \right),$$

$$\mathcal{M}_F = \frac{1}{3} (2M_{GT}^{AA} + M_T^{AA}) + \frac{6\mathbf{g}_{VL}^E}{g_A^2} M_{F, sd}$$

$$+ M_{T, sd}^{AP}) \Big) \Big] \Big],$$

$$+ M_{T, sd}^{AP}) \Big) \Big].$$

$$+ M_{T, sd}^{AP}) \Big) \Big].$$

$$+ M_{T, sd}^{AP}) \Big) \Big].$$

EFT Approach [Cirigliano et al. ArXiv:1806.02780]



$$\begin{aligned}
 \mathcal{M}_{GT} &= M_{GT}^{AA} + M_{GT}^{AP} \\
 \mathcal{M}_T &= M_T^{AP} + M_T^{PP} + M_{GT}^{PP} \\
 \mathcal{M}_{PS} &= \frac{1}{2} M_{AP} + C_8^{(9)\prime} + C_8^{(9)} , \quad \tilde{C}_V^{(9)} = C_7^{(9)} + C_7^{(9)\prime} + C_9^{(9)} + C_9^{(9)\prime} - g_4^{\pi\pi} C_{4L}^{(9)} - g_5^{\pi\pi} C_{5L}^{(9)} - \frac{5}{3} g_1^{\pi\pi} m_\pi^2 \left(C_{1L}^{(9)} + C_{1L}^{(9)\prime} \right) + g_4^{NN} C_{4L}^{(9)} + g_5^{NN} C_{5L}^{(9)} \\
 C_V^{(9)} &= C_6^{(9)} + C_6^{(9)\prime} + C_{2L}^{(9)} + C_{2L}^{(9)\prime} + g_3^{\pi\pi} \left(C_{3L}^{(9)} + C_{3L}^{(9)\prime} \right) \\
 C_{\pi\pi L}^{(9)} &= g_2^{\pi\pi} \left(C_{2L}^{(9)} + C_{1L}^{(9)} \right) \left(C_{1L}^{(9)} + C_{1L}^{(9)\prime} \right) \\
 C_{\pi N L}^{(9)} &= \left(g_1^{\pi N} - \frac{5}{6} g_1^{\pi\pi} \right) \left(C_{1L}^{(9)} + C_{1L}^{(9)\prime} \right) + g_2^{NN} \left(C_{2L}^{(9)} + C_{2L}^{(9)\prime} \right) + g_3^{NN} \left(C_{3L}^{(9)} + C_{3L}^{(9)\prime} \right) + g_4^{NN} \left(C_{4L}^{(9)} + C_{4L}^{(9)\prime} \right) + g_5^{NN} \left(C_{5L}^{(9)} + C_{5L}^{(9)\prime} \right) + M_{T,sd}^{(\pi\pi)} \Big] \\
 C_{NNL}^{(9)} &= g_1^{NN} \left(C_{1L}^{(9)} + C_{1L}^{(9)\prime} \right) \Big|_{L \rightarrow R} \\
 \mathcal{A}_R C_{\{\pi\pi, \pi N, NN\}R} &= C_{\{\pi\pi, \pi N, NN\}L} \Big|_{L \rightarrow R} \cdot \frac{4m_N^2}{6} \left(M_{GT,sd}^{PP} + M_{T,sd}^{PP} \right) \\
 \mathcal{A}_E &= \mathcal{M}_{E,L}^{(6)} \left(C_{VL}^{(6)} \right) \\
 \mathcal{A}_E &= \mathcal{M}_{e,L}^{(6)} \left(C_{VL}^{(6)} \right) \\
 \mathcal{A}_{me} &= \mathcal{M}_{me,L}^{(6)} \left(C_{VL}^{(6)} \right) \\
 \text{Input } \mathcal{A}_M &= \frac{m_N}{m_e} \mathcal{M}_M^{(6)} \left(C_{VL}^{(6)} \right) \\
 \mathcal{M}_{me,R}^{(6)} &= \frac{V_{ud} C_{VR}^{(6)}}{6} \left(\frac{g_V^2}{g_A^2} M_F + \frac{1}{3} \left(M_{GT}^{AA} - 4M_T^{AA} \right) + 3 \left(M_{GT}^{AP} + M_{GT}^{PP} + M_T^{AP} + M_T^{PP} \right) \right. \\
 &\quad \left. - \frac{12g_{VL}^{me}}{g_A^2} M_{F,sd} \right), \\
 \mathcal{M}_{T6} &= M_F - \frac{1}{3} \left(2M_{GT}^{AA} + M_T^{AA} \right) + \frac{6g_{VL}^E}{g_A^2} M_{F,sd} \\
 &\quad - \left(C_{T6}^{(7)} \right)
 \end{aligned}$$

How to distinguish?

Standard or non-standard mechanism?

3 different observables in decay experiments

- 1) Half-Life
- 2) Single Electron Spectra
- 3) Angular Correlation

1) Half-Life → Ratios

NMEs depend on (A,Z)

Study Ratios of Half-Lifes [see Deppisch and Päs arXiv:hep-ph/0612165]

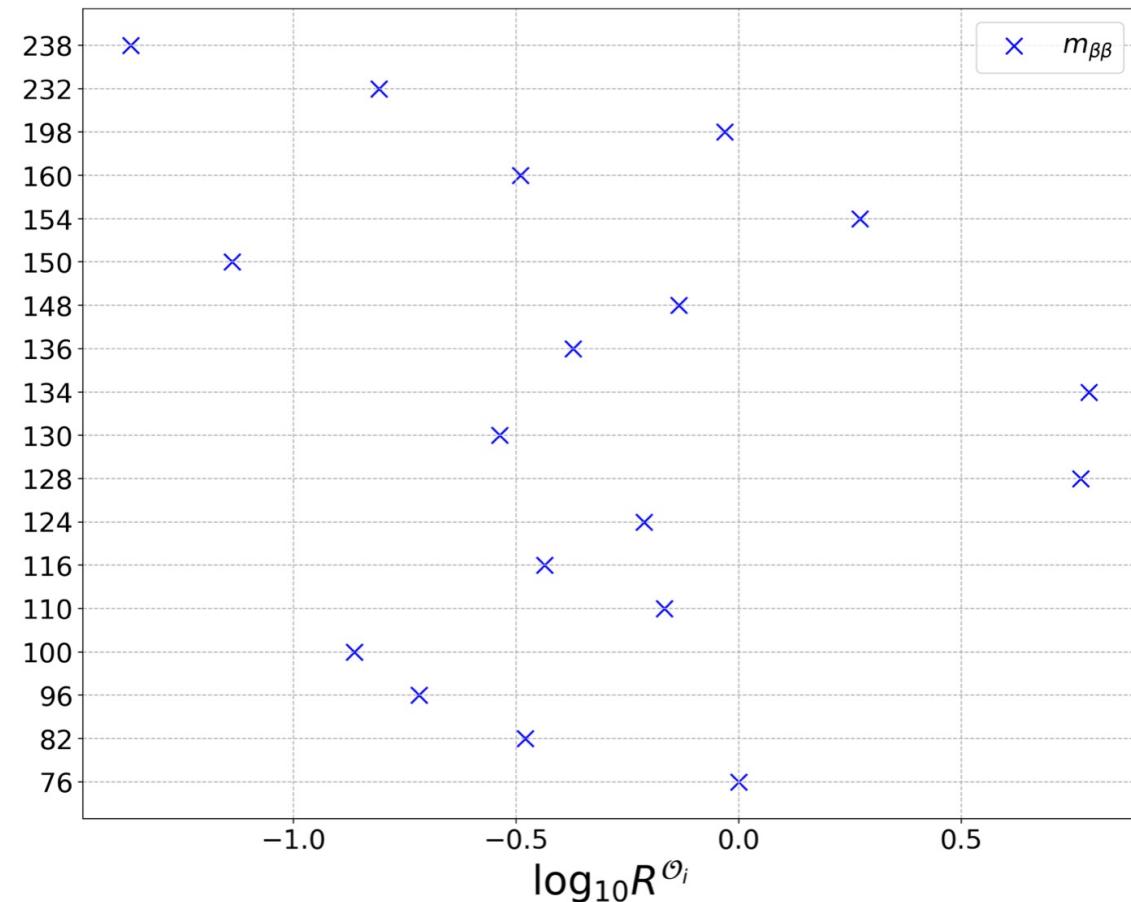
$$R^{\mathcal{O}_i}({}^A X) \equiv \frac{T_{1/2}^{\mathcal{O}_i}({}^A X)}{T_{1/2}^{\mathcal{O}_i}({}^{76} \text{Ge})} = \frac{|\mathcal{M}^{\mathcal{O}_i}({}^{76} \text{Ge})|^2 G^{\mathcal{O}_i}({}^{76} \text{Ge})}{|\mathcal{M}^{\mathcal{O}_i}({}^A X)|^2 G^{\mathcal{O}_i}({}^A X)}$$

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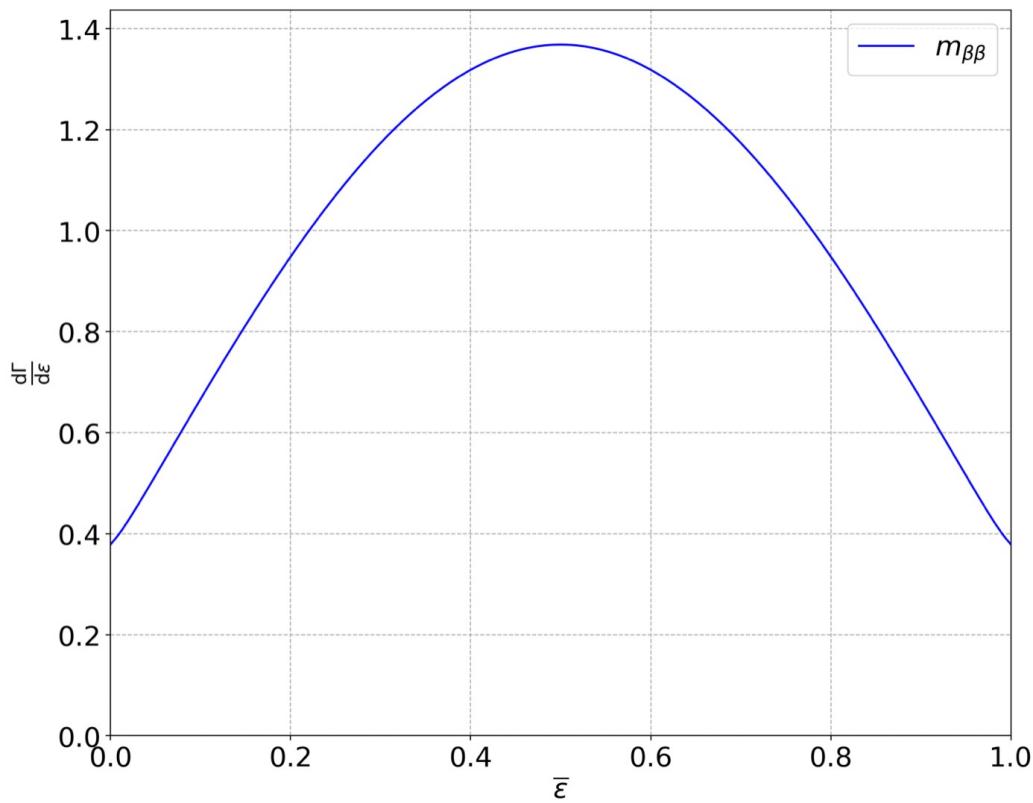
Distinguish 2 operators i, j by

$$R_{ij}({}^A X) = \frac{R^{\mathcal{O}_i}({}^A X)}{R^{\mathcal{O}_j}({}^A X)}$$

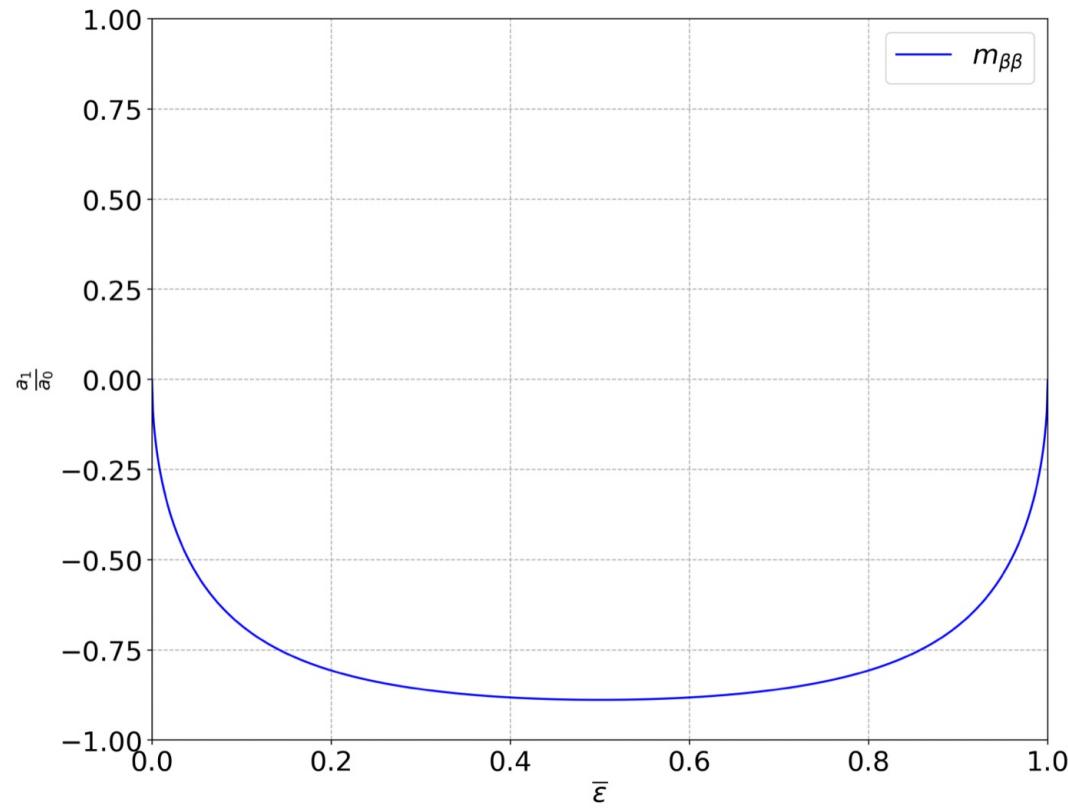
Similar for more complex models

2) + 3) Phase Space Observables

Single Electron Spectra

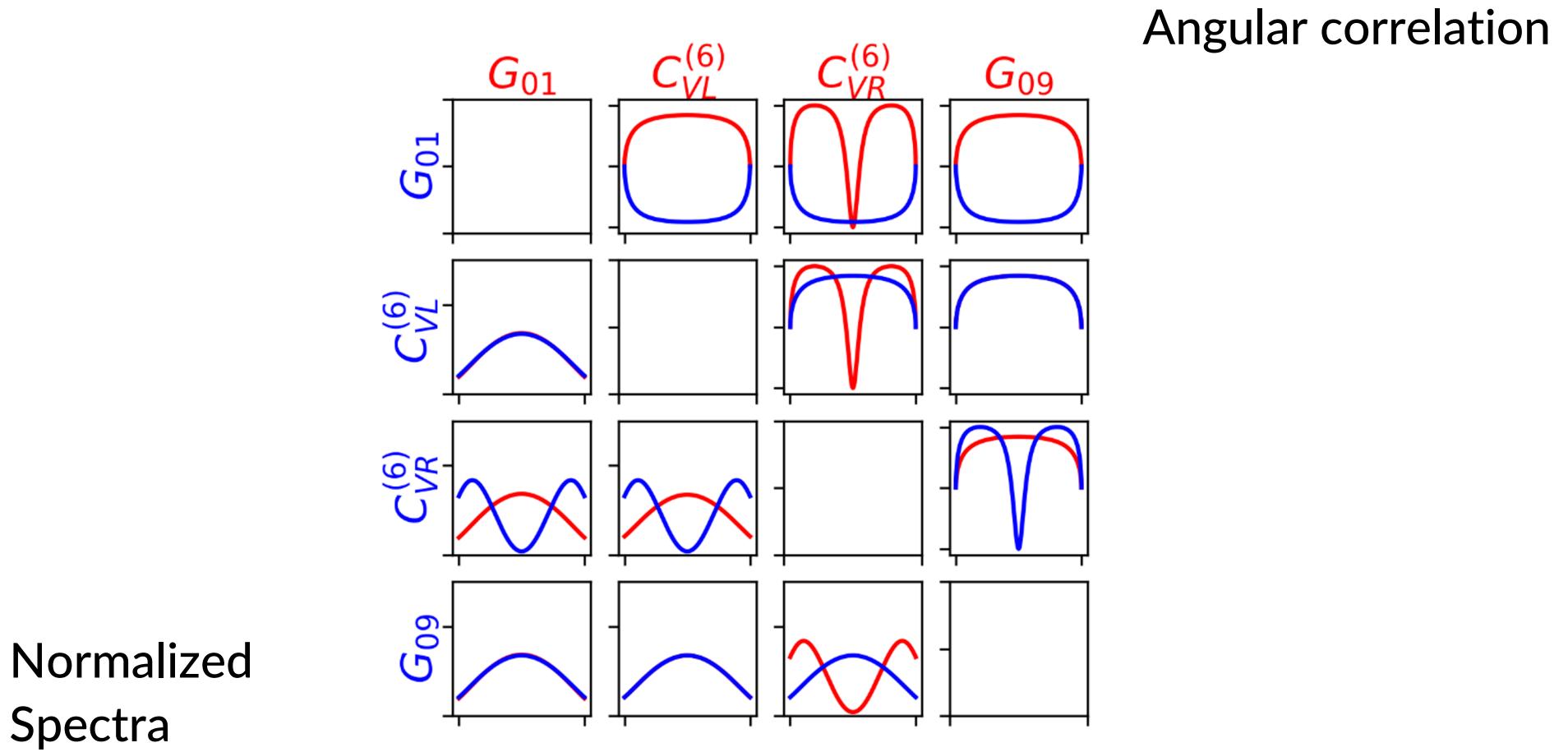


Angular Correlation



2) + 3) Phase Space Observables

→ 4 different groups (plot for ^{136}Xe)



Tool for $0\nu\beta\beta$ -models

Tool to study all possible EFT models:

- $0\nu\beta\beta$ observables
- Distinguishability from standard-mechanism
- Operator Limits

Thank you for attention!